



Limited Operational Impact Study for Generation Interconnection Request

GEN-2011-007

March, 2012
Generation Interconnection



Executive Summary

<OMITTED TEXT> (Customer) has requested an Limited Operation Impact Study under the Southwest Power Pool Open Access Transmission Tariff (OATT) for interconnection of 250.1 MW of wind generation within the balancing authority of Oklahoma Gas & Electric (OKGE) in Canadian County, Oklahoma. Customer has requested this Limited Operation Impact Study (LOIS) to determine the impacts of interconnecting its generating facility to the transmission system before such time that SPP can complete the required interconnection studies. Limited Operation Studies are conducted under GIA Section 5.9.

This study assumed that only the higher queued projects identified in Table 3 of this study might go into service before the completion of all Network Upgrades identified in DISIS-2011-001-1. If any additional generation projects not identified in Table 3 but with queue priority equal to or over GEN-2011-007, those projects listed in Table 4, request to go into commercial operation before all Network Upgrades identified through the DISIS-2011-001-1 study process as required, then this study must be conducted again to determine whether sufficient limited interconnection service exists to interconnect the GEN-2011-007 interconnection request in addition to all higher priority requests in operation or pending operation.

A power flow analysis shows that the Customer's wind facility can interconnect its full 250.1 MW of interconnection capacity. Powerflow analysis was based on both summer and winter peak conditions and light loading cases.

The construction lead time to construct the interconnection substation will be determined by the Transmission Owner during the Facility Study. Any proposed in service date will be contingent upon the completion of the Interconnection Substation.

The wind generation facility was studied as a 250.1 MW with a total of one hundred twenty-two RePower 2.05 MW wind turbine generators. This Impact study addresses the dynamic stability effects of interconnecting the plant to the rest of the OKGE transmission system for the system condition as it will be on December 31, 2012. Two seasonal base cases were used in the study to analyze the stability impacts of the proposed generation facility. The cases studied were modified 2011 summer peak and 2011 winter peak cases that were adjusted to reflect system conditions at the requested in-service date. Each case was modified to include prior queued projects that are listed in the body of the report. Twenty-eight (28) contingencies were identified for use in this study. The RePower 2.05 MW wind turbines were modeled using information provided by the Customer. Stability Analysis indicates the transmission system will remain stable for the studied contingencies for the added generation.

Nothing in this study should be construed as a guarantee of transmission service. If the customer wishes to sell power from the facility, a separate request for transmission service shall be requested on Southwest Power Pool's OASIS by the Customer.

Table of Contents

Executive Summary	i
Table of Contents	ii
Introduction	1
Purpose	1
Facilities	2
Generating Facility	2
Interconnection Facility	2
Powerflow Analysis	4
Stability Analysis	6
Contingencies Simulated.....	6
Further Model Preparation	8
Results	10
FERC LVRT Compliance	11
Conclusion	13

Introduction

<OMITTED TEXT> (Customer) has requested an Limited Operation Impact Study under the Southwest Power Pool Open Access Transmission Tariff (OATT) for interconnection of 250.1 MW of wind generation within the balancing authority of Oklahoma Gas & Electric (OKGE) in Canadian County, Oklahoma. Customer has requested this Limited Operation Impact Study (LOIS) to determine the impacts of interconnecting its generating facility to the transmission system before such time that SPP can complete the required interconnection studies. Limited Operation Studies are conducted under GIA Section 5.9.

This Impact study addresses the dynamic stability effects of interconnecting the plant to the rest of the OKGE transmission system for the system condition as it will be on December 31, 2012. The wind generation facility was studied as a 250.1 MW request with a total of with one hundred twenty-two RePower 2.05 MW wind turbine generators. Two seasonal base cases were used in the study to analyze the stability impacts of the proposed generation facility. The cases studied were modified versions of the 2011 summer peak and 2011 winter peak to reflect the system conditions at the requested in-service date. Each case was modified to include prior queued projects that are listed in the body of the report. Twenty-eight (28) contingencies were identified for this study.

Purpose

The purpose of this Limited Operation Impact Study (LOIS) is to evaluate the impact of the proposed interconnection on the reliability of the Transmission System. The LOIS considers the Base Case as well as all Generating Facilities (and with respect to (b) below, any identified Network Upgrades associated with such higher queued interconnection) that, on the date the LOIS is commenced:

- a) are directly interconnected to the Transmission System;
- b) are interconnected to Affected Systems and may have an impact on the Interconnection Request;
- c) have a pending higher queued Interconnection Request to interconnect to the Transmission System listed in Table 3; or
- d) have no Queue Position but have executed an LGIA or requested that an unexecuted LGIA be filed with FERC.

Any changes to these assumptions, for example, one or more of the previously queued projects not included in this study signing an interconnection agreement, may require a re-study of this request at the expense of the customer.

Nothing in this System Impact Study constitutes a request for transmission service or confers upon the Interconnection Customer any right to receive transmission service.

Facilities

Generating Facility

The project was modeled with the existing plant as two equivalent wind turbine generators of 141.45MW and 108.65MW for a total of 250.1 MW output. The wind turbines are connected to equivalent 0.69/34.5KV generator step units (GSU). The high side of each GSU is connected to a 34.5/345kV substation transformer. A 345kV transmission line connects the Customer’s substation transformer to the POI.

Interconnection Facility

The Point of Interconnection will be at a new 345kV switching station along the Transmission Owners Cimarron-Woodring 345kV transmission line. Figure 1 shows a one-line illustration of the facility and the POI. Figure 2 shows a one-line bus interconnection of the Point of Interconnection.

Cost to interconnect on a limited basis is estimated at \$9,276,873. The construction lead time to construct the interconnection substation will be determined by the Transmission Owner during the Facility Study. Any proposed in service date will be contingent upon the completion of the Interconnection Substation.

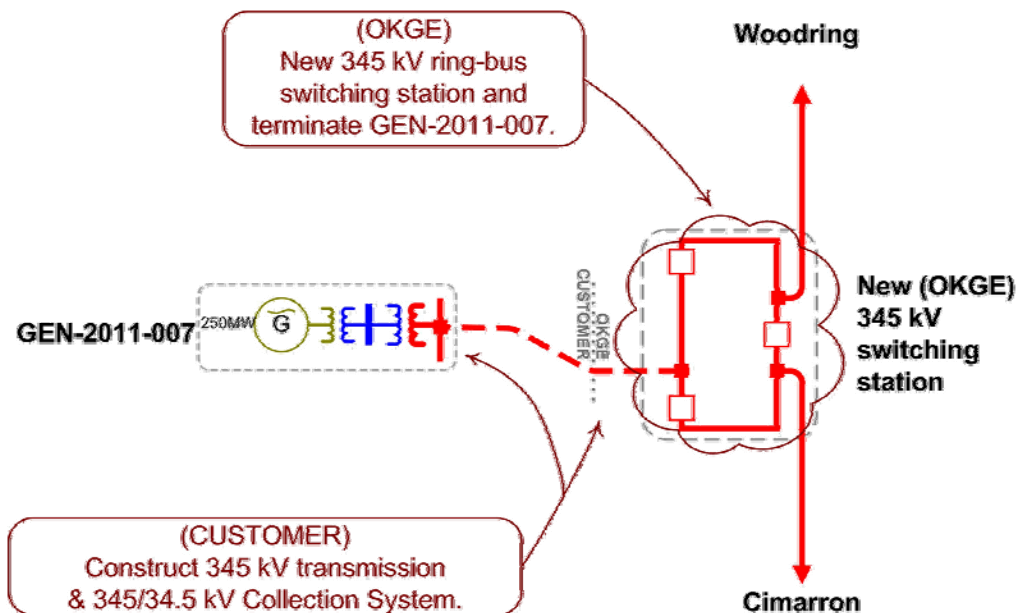


Figure 1: GEN-2011-007 Facility and Proposed Interconnection Configuration

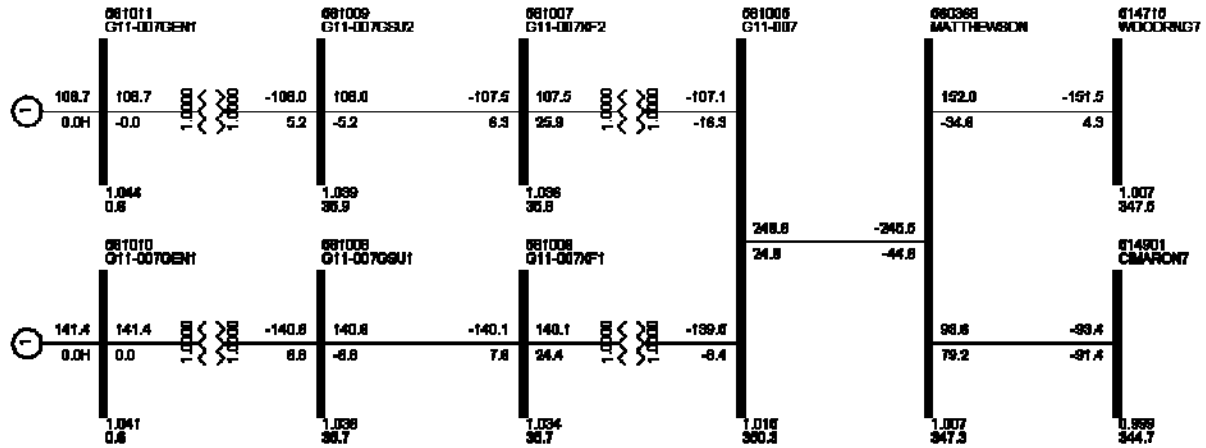


Figure 2: GEN-2011-007 Bus Interconnection

Powerflow Analysis

A powerflow analysis was conducted for the Interconnection Customer's facility using a modified version of the 2012 spring, 2012 summer, and 2012 winter seasonal models. The output of the Interconnection Customer's facility was offset in the model by a reduction in output of existing online SPP generation. This method allows the request to be studied as an Energy Resource (ERIS) Interconnection Request. This analysis was conducted assuming that previous queued requests listed in Table 3 were in-service.

The Southwest Power Pool (SPP) Criteria states that:

“The transmission system of the SPP region shall be planned and constructed so that the contingencies as set forth in the Criteria will meet the applicable NERC Reliability Standards for transmission planning. All MDWG power flow models shall be tested to verify compliance with the System Performance Standards from NERC Table 1 – Category A.”

The ACCC function of PSS/E was used to simulate single contingencies in portions of or all of the control area of OKGE and other control areas within SPP and the resulting data analyzed. This satisfies the “more probable” contingency testing criteria mandated by NERC and the SPP criteria.

Higher queued projects listed in Table 4 were not modeled as in service. If any of these come in service, this study will need to be performed again to determine if any limited interconnection service is available.

The ACCC analysis indicates that the Customer's project can interconnect 250.1 MW of generation into the OKGE transmission system.

Table 1: ACCC Analysis for GEN-2011-007

SEASON	SOURCE	DIRECTION	MONTCOMMONNAME	RATEA	RATEB	TDF	TC%LOADING	MW Available	CONTNAME
			None						

Stability Analysis

Contingencies Simulated

Twenty-eight (28) contingencies were considered for the transient stability simulations. These contingencies included three phase faults and single phase line faults at locations defined by SPP. Single-phase line faults were simulated by applying a fault impedance to the positive sequence network at the fault location to represent the effect of the negative and zero sequence networks on the positive sequence network. The fault impedance was computed to give a positive sequence voltage at the specified fault location of approximately 60% of pre-fault voltage. This method is in agreement with SPP current practice.

The faults that were defined and simulated are listed in Table 2 below.

Table 2: Contingencies Evaluated

Cont. No.	Cont. Name	Description
1.	FLT_01_TATONGA7_WWR DEHV7_345kV_3PH	3 phase fault on the Tatonga (515407) to Woodward EHV (515375) 345kV line, near Tatonga. a. Apply fault at Tatonga 345kV bus. b. Clear fault after 5 cycles by tripping the faulted line. c. Wait 20 cycles, and then re-close the line in (b) back into the fault. d. Leave fault on for 5 cycles, then trip the line in (b) and remove fault.
2.	FLT_02_TATONGA7_WWR DEHV7_345kV_1PH	<i>Single phase fault and sequence like previous</i>
3.	FLT_03_NORTWST7_TATONGA7_345kV_3PH	3 phase fault on the Northwest (514880) to Tatonga (515407) 345kV line, near Northwest. a. Apply fault at Northwest 345kV bus. b. Clear fault after 5 cycles by tripping the faulted line. c. Wait 20 cycles, and then re-close the line in (b) back into the fault. d. Leave fault on for 5 cycles, then trip the line in (b) and remove fault.
4.	FLT_04_NORTWST7_TATONGA7_345kV_1PH	<i>Single phase fault and sequence like previous</i>
5.	FLT_05_CIMARON7_MINCO7_345kV_3PH	3 phase fault on the Cimarron (514901) to Minco (514801) 345kV line, near Cimarron. a. Apply fault at Cimarron 345kV bus. b. Clear fault after 5 cycles by tripping the faulted line. c. Wait 20 cycles, and then re-close the line in (b) back into the fault. d. Leave fault on for 5 cycles, then trip the line in (b) and remove fault.
6.	FLT_06_CIMARON7_MINCO7_345kV_1PH	<i>Single phase fault and sequence like previous</i>
7.	FLT_07_CIMARON7_NORTWST7_345kV_3PH	3 phase fault on the Cimarron (514901) to Northwest (514880) 345kV line, near Cimarron. a. Apply fault at Cimarron 345kV bus. b. Clear fault after 5 cycles by tripping the faulted line. c. Wait 20 cycles, and then re-close the line in (b) back into the fault. d. Leave fault on for 5 cycles, then trip the line in (b) and remove fault.
8.	FLT_08_CIMARON7_NORTWST7_345kV_1PH	<i>Single phase fault and sequence like previous</i>

Cont. No.	Cont. Name	Description
9.	FLT_09_CIMARON7_DRAPER7_345kV_3PH	3 phase fault on the Cimarron (514901) to Draper (514934) 345kV line, near Cimarron. a. Apply fault at Cimarron 345kV bus. b. Clear fault after 5 cycles by tripping the faulted line. c. Wait 20 cycles, and then re-close the line in (b) back into the fault. d. Leave fault on for 5 cycles, then trip the line in (b) and remove fault.
10.	FLT_10_CIMARON7_DRAPER7_345kV_1PH	<i>Single phase fault and sequence like previous</i>
11.	FLT_11_CIMARON7_CIMARON4_345_138kV_3PH	3 phase fault on one of the Cimarron 345kV (514901) to Cimarron 138kV (514898) transformers on the 345kV bus. a. Apply fault at Cimarron 345kV bus. b. Clear fault after 5 cycles by tripping the faulted transformer.
12.	FLT_12_MATTHEWSON_CIMARON7_345kV_3PH	3 phase fault on the Matthewson (560368) to Cimarron (514901) 345kV line, near Matthewson. a. Apply fault at Matthewson 345kV bus. b. Clear fault after 5 cycles by tripping the faulted line. c. Wait 20 cycles, and then re-close the line in (b) back into the fault. d. Leave fault on for 5 cycles, then trip the line in (b) and remove fault.
13.	FLT_13_MATTHEWSON_CIMARON7_345kV_1PH	<i>Single phase fault and sequence like previous</i>
14.	FLT_14_MATTHEWSON_WOODRING7_345kV_3PH	3 phase fault on the Matthewson (560368) to Woodring (514715) 345kV line, near Matthewson. a. Apply fault at Matthewson 345kV bus. b. Clear fault after 5 cycles by tripping the faulted line. c. Wait 20 cycles, and then re-close the line in (b) back into the fault. d. Leave fault on for 5 cycles, then trip the line in (b) and remove fault.
15.	FLT_15_MATTHEWSON_WOODRING7_345kV_1PH	<i>Single phase fault and sequence like previous</i>
16.	FLT_16_WOODRING7_SOONER7_345kV_3PH	3 phase fault on the Woodring (514715) to Sooner (514803) 345kV line, near Woodring. a. Apply fault at Woodring 345kV bus. b. Clear fault after 5 cycles by tripping the faulted line. c. Wait 20 cycles, and then re-close the line in (b) back into the fault. d. Leave fault on for 5 cycles, then trip the line in (b) and remove fault.
17.	FLT_17_WOODRING7_SOONER7_345kV_1PH	<i>Single phase fault and sequence like previous</i>
18.	FLT_18_WOODRING7_GEN2008013TAP_345kV_3PH	3 phase fault on the Woodring (514715) to GEN-2008-013 Tap (579406) 345kV line, near Woodring. a. Apply fault at Woodring 345kV bus. b. Clear fault after 5 cycles by tripping the faulted line. c. Wait 20 cycles, and then re-close the line in (b) back into the fault. d. Leave fault on for 5 cycles, then trip the line in (b) and remove fault.
19.	FLT_19_WOODRING7_GEN2008013TAP_345kV_1PH	<i>Single phase fault and sequence like previous</i>
20.	FLT_20_GEN2008013TAP_GEN2007025TAP_345kV_3PH	3 phase fault on the GEN-2008-013 Tap (579406) to GEN-2007-025 Tap (579267) 345kV line, near GEN-2008-013 Tap. a. Apply fault at GEN-2008-013 Tap 345kV bus. b. Clear fault after 5 cycles by tripping the faulted line. c. Wait 20 cycles, and then re-close the line in (b) back into the fault. d. Leave fault on for 5 cycles, then trip the line in (b) and remove fault.
21.	FLT_21_GEN2008013TAP_GEN2007025TAP_345kV_1PH	<i>Single phase fault and sequence like previous</i>

Cont. No.	Cont. Name	Description
22.	FLT_22_GEN2007025TAP_WICHITA7_345kV_3PH	3 phase fault on the GEN-2007-025 Tap (579267) to Wichita (532796) 345kV line, near GEN-2007-025 Tap. a. Apply fault at GEN-2007-025 Tap 345kV bus. b. Clear fault after 5 cycles by tripping the faulted line. c. Wait 20 cycles, and then re-close the line in (b) back into the fault. d. Leave fault on for 5 cycles, then trip the line in (b) and remove fault.
23.	FLT_23_GEN2007025TAP_WICHITA7_345kV_1PH	<i>Single phase fault and sequence like previous</i>
24.	FLT_24_WOODRNG7_WOODRNG4_345_138kV_3PH	3 phase fault on one of the Woodring 345kV (514715) to Woodring 138kV (514714) transformers on the 345kV bus. a. Apply fault at Woodring 345kV bus. b. Clear fault after 5 cycles by tripping the faulted transformer.
25.	FLT_25_WICHITA7_BENTON7_345kV_3PH	3 phase fault on the Wichita (532796) to Benton (532791) 345kV line, near Woodring. a. Apply fault at Woodring 345kV bus. b. Clear fault after 5 cycles by tripping the faulted line. c. Wait 20 cycles, and then re-close the line in (b) back into the fault. d. Leave fault on for 5 cycles, then trip the line in (b) and remove fault.
26.	FLT_26_WICHITA7_BENTON7_345kV_1PH	<i>Single phase fault and sequence like previous</i>
27.	FLT_27_SOONER7_SPRNGCK7_345kV_3PH	3 phase fault on the Sooner (514803) to Spring Creek (514881) 345kV line, near Sooner. a. Apply fault at Sooner 345kV bus. b. Clear fault after 5 cycles by tripping the faulted line. c. Wait 20 cycles, and then re-close the line in (b) back into the fault. d. Leave fault on for 5 cycles, then trip the line in (b) and remove fault.
28.	FLT_28_SOONER7_SPRNGCK7_345kV_1PH	<i>Single phase fault and sequence like previous</i>
29.	FLT_29_WOODRNG4_OTTER4_138kV_3PH	3 phase fault on the Woodring (514714) to Otter (514708) 138kV line, near Woodring. a. Apply fault at Woodring 138kV bus. b. Clear fault after 5 cycles by tripping the faulted line. c. Wait 20 cycles, and then re-close the line in (b) back into the fault. d. Leave fault on for 5 cycles, then trip the line in (b) and remove fault.
30.	FLT_30_WOODRNG4_OTTER4_138kV_1PH	<i>Single phase fault and sequence like previous</i>
31.	FLT_31_CIMARRON4_ELRENO4_138kV_3PH	3 phase fault on the Cimarron (514898) to El Reno (514819) 138kV line, near Cimarron. a. Apply fault at Cimarron 138kV bus. b. Clear fault after 5 cycles by tripping the faulted line. c. Wait 20 cycles, and then re-close the line in (b) back into the fault. d. Leave fault on for 5 cycles, then trip the line in (b) and remove fault.
32.	FLT_32_CIMARRON4_ELRENO4_138kV_1PH	<i>Single phase fault and sequence like previous</i>

Further Model Preparation

The base cases contain prior queued projects as shown in Table 3.

The wind generation from the study customer and the previously queued customers were dispatched into the SPP footprint.

Initial simulations were carried out on both base cases and cases with the added generation for a no-disturbance run of 20 seconds to verify the numerical stability of the model. All cases were confirmed to be stable.

Table 3: Prior Queued Projects Included

Project	MW
GEN-2001-014	96
GEN-2001-037	100
GEN-2005-008	120
GEN-2006-024S	19.8
GEN-2006-046	131
GEN-2007-025	300
GEN-2007-043	200
GEN-2007-050	170
GEN-2008-003	101
GEN-2008-013	300
GEN-2008-044	197.8
GEN-2010-011	29.7
GEN-2010-040	300
GEN-2011-010	100.8

The projects listed in Table 4 are higher or equally queued projects that are not included in this analysis. If any of these projects come into service, this study will need to be re-performed to determine if any limited service is available.

Table 4: Prior Queued Projects Not Included

Project	MW
GEN-2005-005	18
GEN-2007-006	160
GEN-2007-021	201
GEN-2007-044	300
GEN-2007-051	200
GEN-2007-062	765
GEN-2008-019	300
GEN-2008-029	250.5
GEN-2011-019	299
GEN-2011-020	299
GEN-2011-024	299

Results

Results of the stability analysis are summarized in Table 5. These results are valid for GEN-2011-007 interconnecting with a generation amount of 250.1 MW. The results indicate that for all contingencies studied the transmission system remains stable.

Table 5: Contingencies Evaluated

Cont. No.	Cont. Name	Description	2011 Summer	2011 Winter
1.	FLT_01_TATONGA7_WWR DEHV7_345kV_3PH	3 phase fault on the Tatonga (515407) to Woodward EHV (515375) 345kV line, near Tatonga.	Stable	Stable
2.	FLT_02_TATONGA7_WWR DEHV7_345kV_1PH	<i>Single phase fault and sequence like previous</i>	Stable	Stable
3.	FLT_03_NORTWST7_TATONGA7_345kV_3PH	3 phase fault on the Northwest (514880) to Tatonga (515407) 345kV line, near Northwest.	Stable	Stable
4.	FLT_04_NORTWST7_TATONGA7_345kV_1PH	<i>Single phase fault and sequence like previous</i>	Stable	Stable
5.	FLT_05_CIMARON7_MINCO7_345kV_3PH	3 phase fault on the Cimarron (514901) to Minco (514801) 345kV line, near Cimarron.	Stable	Stable
6.	FLT_06_CIMARON7_MINCO7_345kV_1PH	<i>Single phase fault and sequence like previous</i>	Stable	Stable
7.	FLT_07_CIMARON7_NORTWST7_345kV_3PH	3 phase fault on the Cimarron (514901) to Northwest (514880) 345kV line, near Cimarron.	Stable	Stable
8.	FLT_08_CIMARON7_NORTWST7_345kV_1PH	<i>Single phase fault and sequence like previous</i>	Stable	Stable
9.	FLT_09_CIMARON7_DRAPER7_345kV_3PH	3 phase fault on the Cimarron (514901) to Draper (514934) 345kV line, near Cimarron.	Stable	Stable
10.	FLT_10_CIMARON7_DRAPER7_345kV_1PH	<i>Single phase fault and sequence like previous</i>	Stable	Stable
11.	FLT_11_CIMARON7_CIMARON4_345_138kV_3PH	3 phase fault on one of the Cimarron 345kV (514901) to Cimarron 138kV (514898) transformers on the 345kV bus.	Stable	Stable
12.	FLT_12_MATTHEWSON_CIMARON7_345kV_3PH	3 phase fault on the Matthewson (560368) to Cimarron (514901) 345kV line, near Matthewson.	Stable	Stable
13.	FLT_13_MATTHEWSON_CIMARON7_345kV_1PH	<i>Single phase fault and sequence like previous</i>	Stable	Stable
14.	FLT_14_MATTHEWSON_WOODRNG7_345kV_3PH	3 phase fault on the Matthewson (560368) to Woodring (514715) 345kV line, near Matthewson.	Stable	Stable
15.	FLT_15_MATTHEWSON_WOODRNG7_345kV_1PH	<i>Single phase fault and sequence like previous</i>	Stable	Stable
16.	FLT_16_WOODRNG7_SOONER7_345kV_3PH	3 phase fault on the Woodring (514715) to Sooner (514803) 345kV line, near Woodring.	Stable	Stable
17.	FLT_17_WOODRNG7_SOONER7_345kV_1PH	<i>Single phase fault and sequence like previous</i>	Stable	Stable
18.	FLT_18_WOODRNG7_GEN2008013TAP_345kV_3PH	3 phase fault on the Woodring (514715) to GEN-2008-013 Tap (579406) 345kV line, near Woodring.	Stable	Stable
19.	FLT_19_WOODRNG7_GEN2008013TAP_345kV_1PH	<i>Single phase fault and sequence like previous</i>	Stable	Stable
20.	FLT_20_GEN2008013TAP_GEN2007025TAP_345kV_3PH	3 phase fault on the GEN-2008-013 Tap (579406) to GEN-2007-025 Tap (579267) 345kV line, near GEN-2008-013 Tap.	Stable	Stable

Cont. No.	Cont. Name	Description	2011 Summer	2011 Winter
21.	FLT_21_GEN2008013TAP_GEN2007025TAP_345kV_1PH	Single phase fault and sequence like previous	Stable	Stable
22.	FLT_22_GEN2007025TAP_WICHITA7_345kV_3PH	3 phase fault on the GEN-2007-025 Tap (579267) to Wichita (532796) 345kV line, near GEN-2007-025 Tap.	Stable	Stable
23.	FLT_23_GEN2007025TAP_WICHITA7_345kV_1PH	Single phase fault and sequence like previous	Stable	Stable
24.	FLT_24_WOODRNG7_WOODRNG4_345_138kV_3PH	3 phase fault on one of the Woodring 345kV (514715) to Woodring 138kV (514714) transformers on the 345kV bus.	Stable	Stable
25.	FLT_25_WICHITA7_BENTON7_345kV_3PH	3 phase fault on the Wichita (532796) to Benton (532791) 345kV line, near Woodring.	Stable	Stable
26.	FLT_26_WICHITA7_BENTON7_345kV_1PH	Single phase fault and sequence like previous	Stable	Stable
27.	FLT_27_SOONER7_SPRNGCK7_345kV_3PH	3 phase fault on the Sooner (514803) to Spring Creek (514881) 345kV line, near Sooner.	Stable	Stable
28.	FLT_28_SOONER7_SPRNGCK7_345kV_1PH	Single phase fault and sequence like previous	Stable	Stable
29.	FLT_29_WOODRNG4_OTTER4_138kV_3PH	3 phase fault on the Woodring (514714) to Otter (514708) 138kV line, near Woodring.	Stable	Stable
30.	FLT_30_WOODRNG4_OTTER4_138kV_1PH	Single phase fault and sequence like previous	Stable	Stable
31.	FLT_31_CIMARON4_ELRENO4_138kV_3PH	3 phase fault on the Cimarron (514898) to El Reno (514819) 138kV line, near Cimarron.	Stable	Stable
32.	FLT_32_CIMARON4_ELRENO4_138kV_1PH	Single phase fault and sequence like previous	Stable	Stable

FERC LVRT Compliance

FERC Order #661A places specific requirements on wind farms through its Low Voltage Ride Through (LVRT) provisions. For Interconnection Agreements signed after December 31, 2006, wind farms shall stay on line for faults at the POI that draw the voltage down at the POI to 0.0 pu.

Fault contingencies were developed to verify that the wind farm will remain on line when the POI voltage is drawn down to 0.0 pu. These contingencies are shown in Table 6.

Table 6: Contingencies Evaluated

Cont. Name	Description
FLT_12_MATTHEWSON_CIMARON7_345kV_3PH	3 phase fault on the Matthewson (560368) to Cimarron (514901) 345kV line, near Matthewson. a. Apply fault at Matthewson 345kV bus. b. Clear fault after 5 cycles by tripping the faulted line. c. Wait 20 cycles, and then re-close the line in (b) back into the fault. d. Leave fault on for 5 cycles, then trip the line in (b) and remove fault.

Cont. Name	Description
FLT_14_MATTHEWSON_WOODRNG7_345kV_3PH	<p>3 phase fault on the Matthewson (560368) to Woodring (514715) 345kV line, near Matthewson.</p> <ol style="list-style-type: none">Apply fault at Matthewson 345kV bus.Clear fault after 5 cycles by tripping the faulted line.Wait 20 cycles, and then re-close the line in (b) back into the fault.Leave fault on for 5 cycles, then trip the line in (b) and remove fault.

The prior queued project wind farms remained online for the fault contingencies described in this section and for all the fault contingencies described in the Contingencies Simulated section. GEN-2011-007 is found to be in compliance with FERC Order #661A.

Conclusion

<OMITTED TEXT> (Customer) has requested a Limited Operation Impact Study for limited interconnection service of 250.1 MW of wind generation within the balancing authority of Oklahoma Gas & Electric (OKGE) in Canadian County, Oklahoma, in accordance with section 5.9 of the Standard Generation Interconnection Procedures Agreement (GIA) in the SPP OATT.

Power flow analysis showed that the Customer's wind facility can interconnect 250.1 MW of wind generation. The construction lead time to construct the interconnection substation will be determined by the Transmission Owner during the Facility Study. Any proposed in service date will be contingent upon the completion of the Interconnection Substation.

The stability analysis results of this study show that the wind generation facility and the transmission system remain stable for all contingencies studied. Also, GEN-2011-007 is found to be in compliance with FERC Order #661A.

The projects listed in Table 4 are higher or equally queued projects that are not included in this analysis. If any of these projects come into service, this study will need to be re-performed to determine if any limited interconnection service is available.

The estimates do not include any costs associated with the deliverability of the energy to final customers. These costs are determined by separate studies if the Customer requests transmission service through Southwest Power Pool's OASIS. It should be noted that the models used for simulation do not contain all SPP transmission service.